
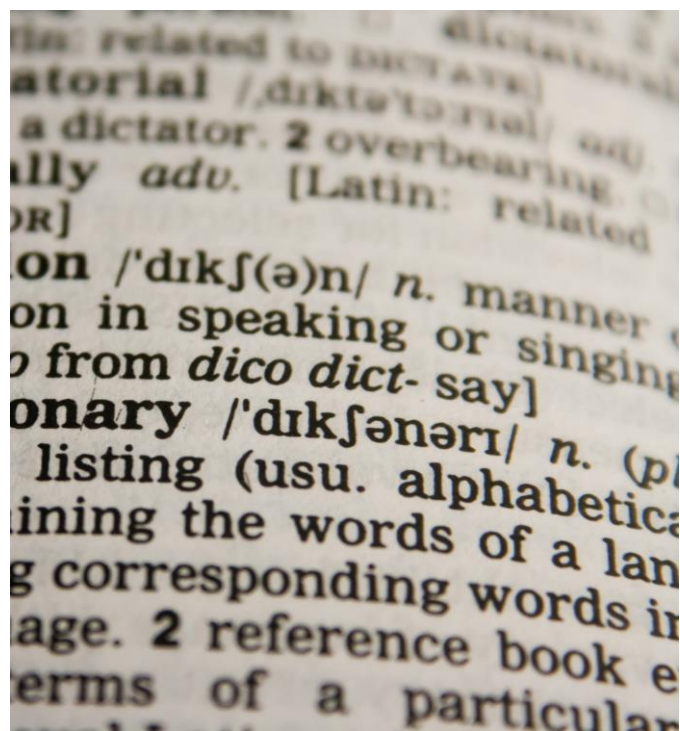


# Kinematics




1

## DEFINITIONS

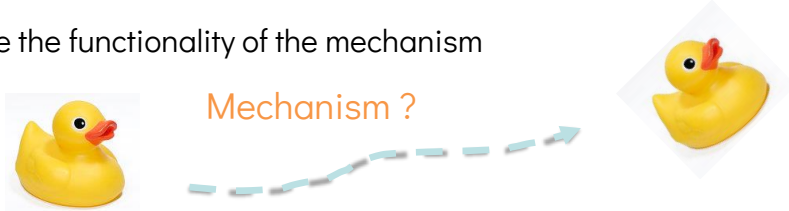



2

# Kinematics

- **Kinematics**: develop various means of transforming motion to achieve a specific task needed in applications

→ ensure the functionality of the mechanism



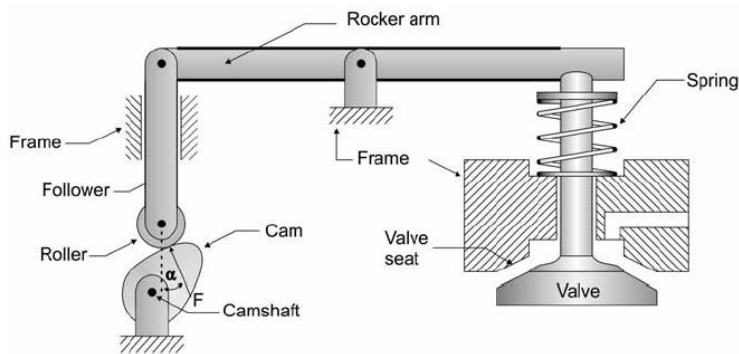
- **Dynamics**: behavior of a given machine or mechanism when subjected to dynamic forces

→ verify the acceptability of induced forces in parts

3

3

## Example : cam operating valve

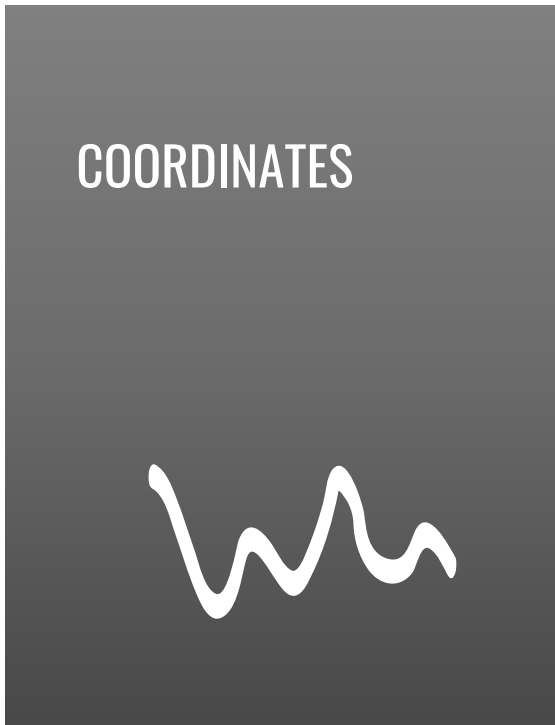


**Kinematical analysis** : satisfy functional requirements for valve displacements.

**Dynamic analysis** : compute forces in the system as a function of time.

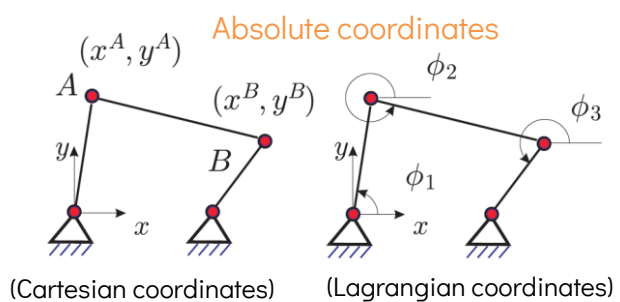
4

4

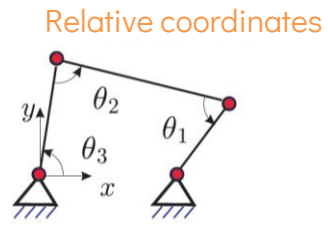


5

## Choice of coordinates



- Absolute vs relative
- Choice is not unique
- How many coordinates ?  
(Efficiency vs simplicity)
- How many constraints ?



→ What is the best choice ?

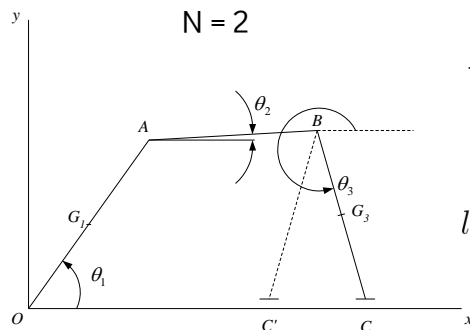
6

6

## Coordinates and constraints

- $N$  = number of **DOFs**: minimum number of coordinates required to fully describe the configuration of a system
- Number of **coordinates**:  $q \geq N$

→ We have to find  $p=q-N$  relationships



Option 1:  $q = 3 : \theta_1, \theta_2, \theta_3$

→  $p = 3 - 2 = 1$

$$l \sin \theta_3 = -l \sin \theta_1 - l \sin \theta_2 \quad | \quad y_C = 0$$

7

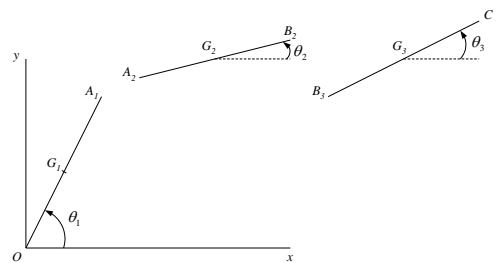
7

## Coordinates and constraints

Option 2:  $q = 7$ :

$$\theta_1, \theta_2, \theta_3, x_{G_2}, y_{G_2}, x_{G_3}, y_{G_3} \quad \rightarrow \quad p = 7 - 2 = 5$$

$$\begin{aligned} 1) \quad & l \cos \theta_1 = x_2 - \frac{l}{2} \cos \theta_2 \quad | \quad A_1 = A_2 \\ 2) \quad & l \sin \theta_1 = y_2 - \frac{l}{2} \sin \theta_2 \\ 3) \quad & x_2 + \frac{l}{2} \cos \theta_2 = x_3 - \frac{l}{2} \cos \theta_3 \quad | \quad B_2 = B_3 \\ 4) \quad & y_2 + \frac{l}{2} \sin \theta_2 = y_3 - \frac{l}{2} \sin \theta_3 \\ 5) \quad & y_3 + \frac{l}{2} \sin \theta_3 = 0 \quad | \quad y_C = 0 \end{aligned}$$



8

8

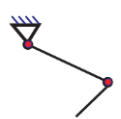


9

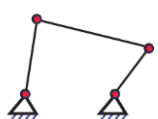
## Number of DOFS

- Number of closed loops:  
 $l$  number of joints  
 $n$  number of bodies

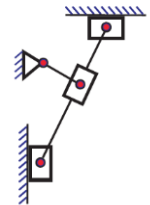
$$b = l - n$$



$$b = 0 (l = 2, n = 2)$$



$$b = 1 (l = 4, n = 3)$$



$$b = 2 (l = 7, n = 5)$$

- Number of DOFs (3D):  
 where  $v_i$  is the number of DOFS at joint  $i$

$$N = \sum_{i=1}^l v_i - 6b$$

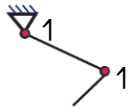
10

10

## Number of DOFS

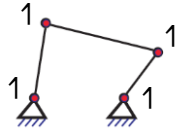
- Number of DOFs (2D):  
where  $v_i$  is the number of DOFS at joint  $i$

$$N = \sum_{i=1}^l v_i - 3b$$



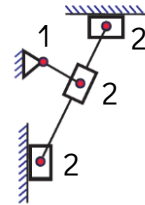
$$b = 0 (l = 2, n = 2)$$

$$N = 1 + 1 - 0 = 2$$



$$b = 1 (l = 4, n = 3)$$

$$N = 4 * 1 - 3 = 1$$



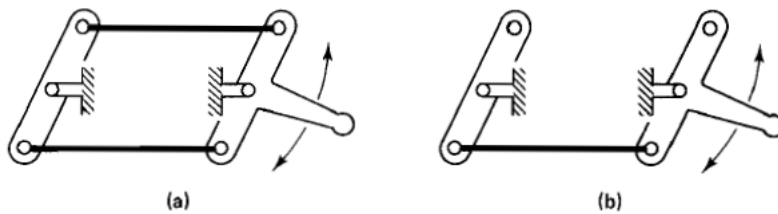
$$b = 2 (l = 7, n = 5)$$

$$N = 3 * 2 + 1 - 6 = 1$$

11

11

## Redundant constraints



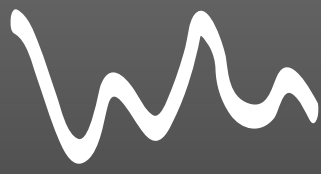
A constraint that can be removed without changing the kinematics is called **redundant**.

→ Not taken into account in the calculation of the number of DOFs.

12

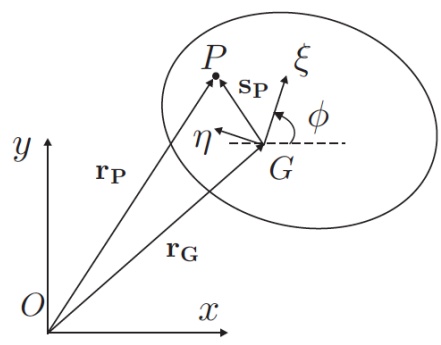
12

# CONSTRAINT EQUATIONS FOR PLANAR JOINTS



13

## Constraint equations : single body revolute joint



$$\bar{r}_P = \bar{r}_G + A\bar{s}_P$$

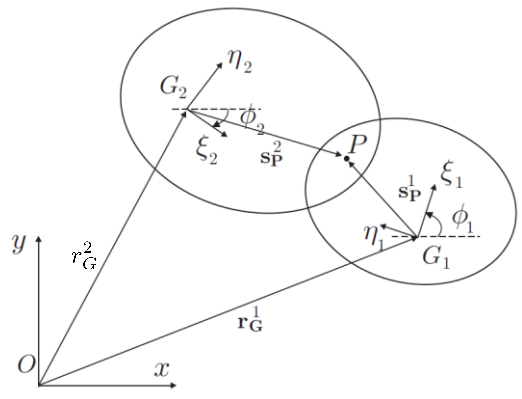


$$A = \begin{bmatrix} \cos \phi & -\sin \phi \\ \sin \phi & \cos \phi \end{bmatrix}$$

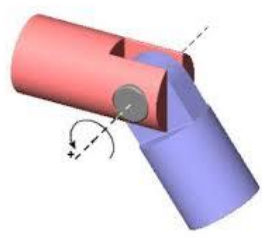
14

14

Constraint equations : two bodies revolute joint



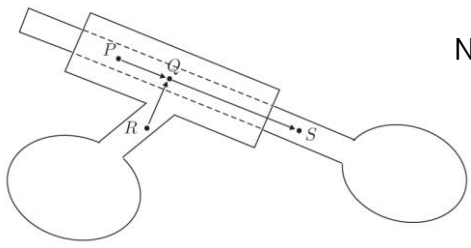
$$\bar{r}_G^1 + A_1 \bar{s}_P^1 = \bar{r}_G^2 + A_2 \bar{s}_P^2$$



15

15

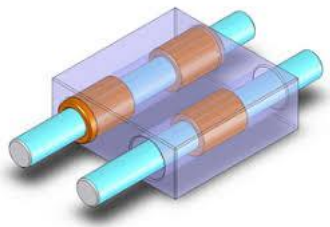
Constraint equations : translation joint



No rotation in the plane between the two bodies

$$\overline{PQ} \times \overline{QS} = 0$$

or 
$$\overline{RQ} \cdot \overline{QS} = 0$$

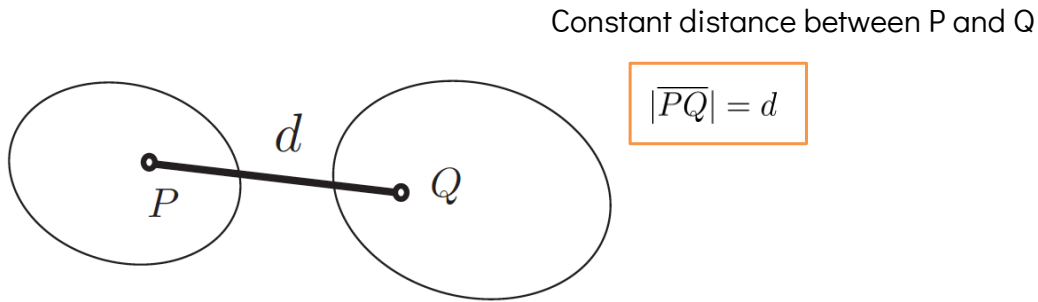


16

16



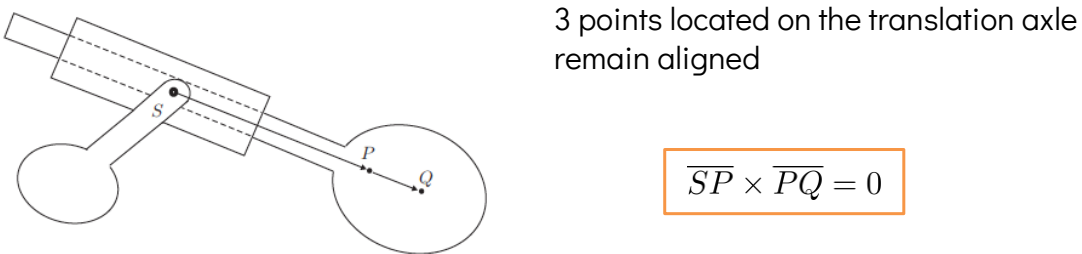
## Constraint equations : revolute-revolute joint



17

17

## Constraint equations : revolute-translation joint

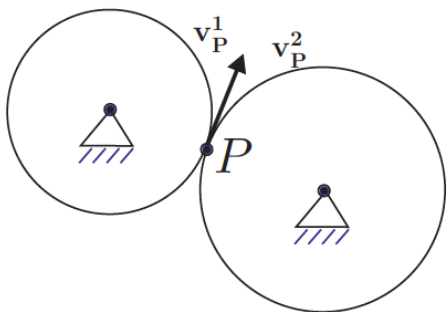


Rotation around S and translation

18

18

## Constraint equations : spur gears



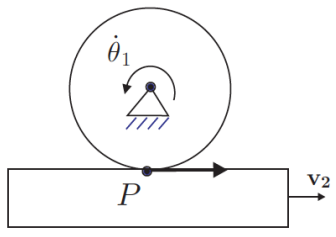
$$\vec{v}_P^1 = \vec{v}_P^2$$

$$\longrightarrow R_1 \dot{\theta}_1 = R_2 \dot{\theta}_2$$

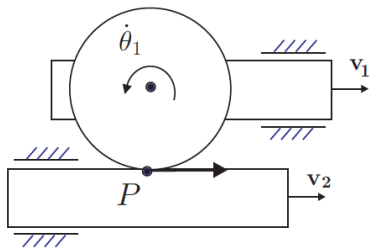
19

19

## Constraint equations : rack and pinion



$$R_1 \dot{\theta}_1 = v_2$$

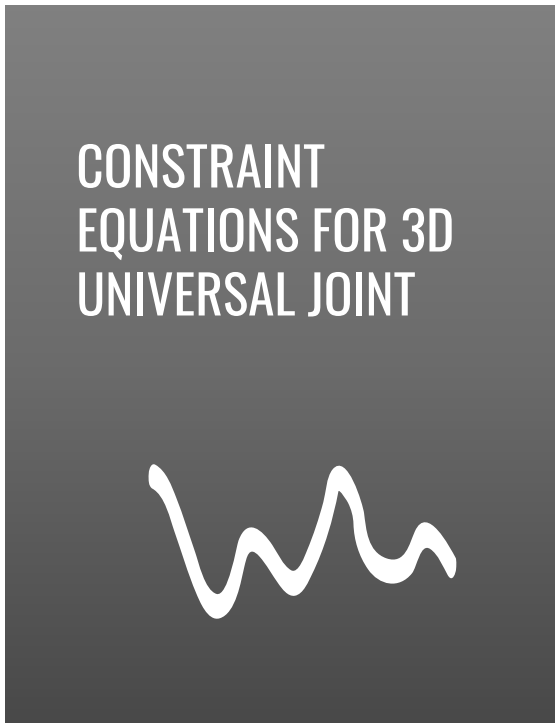


$$v_1 + R_1 \dot{\theta}_1 = v_2$$



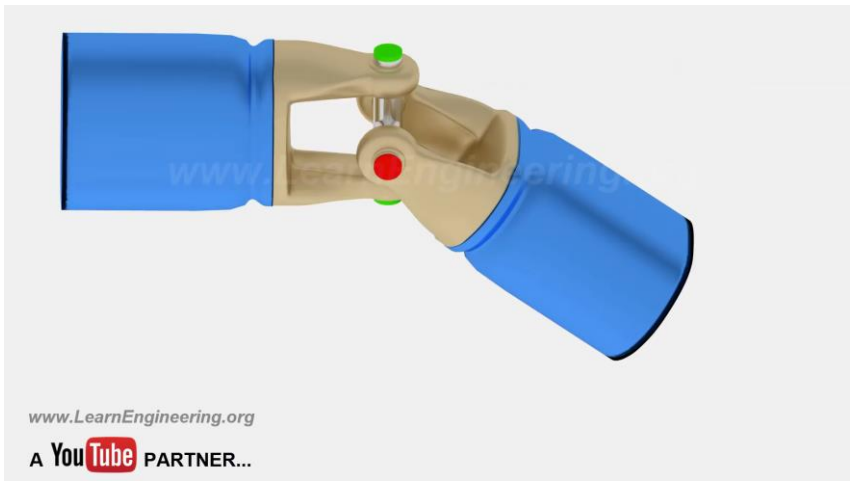
20

20



21

Constraint equations : universal joints

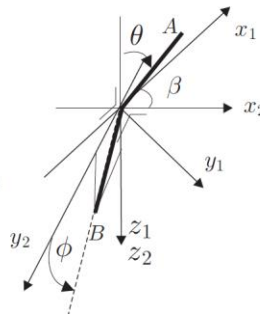
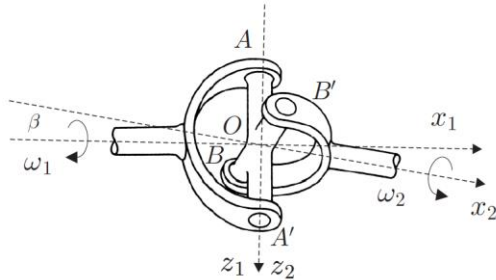


<https://www.youtube.com/watch?v=LCMZz6YhbOQ>

22

22

## Universal joint equations



$$\begin{aligned} \overline{OA} &= \cos \theta \bar{I}_{z_1} + \sin \theta \bar{I}_{y_1} \\ \overline{OB} &= \cos \phi \bar{I}_{y_2} + \sin \phi \bar{I}_{z_2} \end{aligned}$$

$$\overline{OA} \cdot \overline{OB} = 0 \quad \bar{I}_{y_1} \cdot \bar{I}_{y_2} = \cos \beta \quad \bar{I}_{z_1} \cdot \bar{I}_{y_2} = 0 \quad \bar{I}_{z_2} \cdot \bar{I}_{y_1} = 0$$

$$-\cos \theta \sin \phi + \cos \beta \sin \theta \cos \phi = 0 \quad \longrightarrow \quad \tan \phi = \cos \beta \tan \theta$$

23

23

## Universal joint equations

$$\tan \phi = \cos \beta \tan \theta \quad \text{Differentiation:} \quad \frac{1}{\cos^2 \phi} \dot{\phi} = \frac{\cos \beta}{\cos^2 \theta} \dot{\theta}$$

$$\frac{1}{\cos^2 \phi} = 1 + \tan^2 \phi = 1 + \cos^2 \beta \tan^2 \theta$$

$$\omega_2 = \frac{\omega_1 \cos \beta}{1 - \sin^2 \beta \sin^2 \theta}$$

$$\beta \ll$$

Transmission is not uniform unless the two axles are aligned

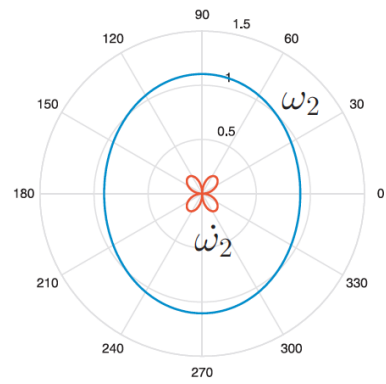
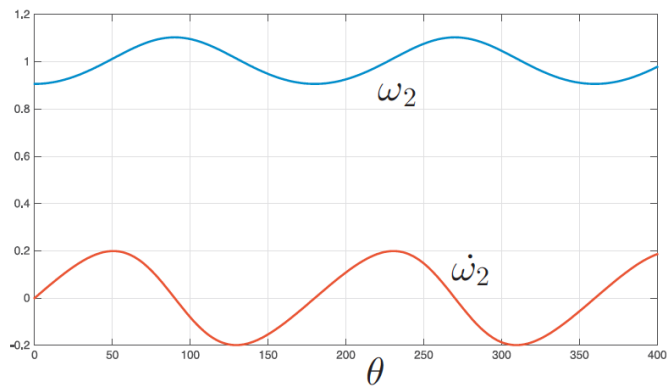
$$\dot{\omega}_2 = \frac{\omega_1^2 \sin^2 \beta \cos \beta \sin 2\theta}{(1 - \sin^2 \beta \sin^2 \theta)^2}$$

24

24

# Universal joint equations

$\beta = 25^\circ$  → 10% variation of  $\omega_2$



25

25